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# Wakes behind wings

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#### European projects

- "C-Wake" (Wake Vortex Characterisation & Control, 2000-2003)
- "FAR-Wake" (Fundamental Research on Aircraft Wake Phenomena, 2005-2008)

Collaborations with Airbus & Eurocopter



## Aircraft wake vortices (examples)





## Aircraft wake vortices (examples)





# Visualisations of aircraft trailing wakes





SEMPRE A BORDO. SEMPRE REFRESCANTE.

## Wing tip and flap tip vortices





## Wing tip vortex in wind tunnel





## Wing tip vortices in catapult facility



Source: ONERA Lille



http://www.onera.fr/cahierdelabo/english/asub8.htm





#### Visualisations of aircraft trailing wakes



Higuchi (1993)

Photo: Cessna Aircraft Company



- danger for following aircraft (downwash, roll)
- minimum separation distances  $\rightarrow$  limits airport capacity



## Rules for separation distances (before A380)

(source: International Civil Aviation Organization ICAO)





## Airbus A380



	A380	B747
wing span	79.8 m	64.4 m
MTOW	560 t	400 t





## Current rules for separation distances



![](_page_12_Picture_2.jpeg)

#### Wakes behind rotating wings

![](_page_13_Picture_1.jpeg)

- helicopters
- propellers
- wind turbines

![](_page_13_Picture_5.jpeg)

![](_page_13_Picture_6.jpeg)

Hand *et al*. (2001)

![](_page_13_Picture_8.jpeg)

Senocak et al. (2002)

![](_page_13_Picture_10.jpeg)

![](_page_13_Picture_11.jpeg)

#### Wakes behind rotating wings

#### wind turbines

 destabilisation/decay of the helical vortex wake

#### helicopters

 transition from helical wake to Vortex Ring State (VRS) in steep descent

![](_page_14_Picture_5.jpeg)

![](_page_14_Picture_6.jpeg)

# **Overview**

#### Basic elements of vortex dynamics and wing wakes

- Vorticity/circulation, vortices, lifting surface, wake vortex systems
- Merging of co-rotating vortices
- Three-dimensional instabilities
  - Long wavelength (Crow instability)
  - Medium wavelength
  - Short wavelength (elliptic instability)
- Vortex reconnection
- Meandering
- Pairing instability of helical vortices

![](_page_15_Picture_11.jpeg)

#### **Nomenclature and definitions**

> velocity 
$$\vec{u} = [u(x, y, z, t), v(x, y, z, t), w(x, y, z, t)]$$

$$\Rightarrow \text{ vorticity} \qquad \vec{\omega} = \vec{\nabla} \times \vec{u} = \left(\frac{\partial v}{\partial z} - \frac{\partial w}{\partial y}, \frac{\partial w}{\partial x} - \frac{\partial u}{\partial z}, \frac{\partial u}{\partial y} - \frac{\partial v}{\partial x}\right) \vec{\nabla} = \left(\frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z}\right) \qquad \Rightarrow \quad \vec{\nabla} \cdot \vec{\omega} = 0$$

$$\succ \text{ circulation } \Gamma = \oint_C \vec{u} \cdot d\vec{l}$$
$$= \int_S \vec{\omega} \cdot d\vec{S}$$

![](_page_16_Picture_4.jpeg)

#### Common hypotheses

#### Newtonian fluid

**└→** stresses ∝ velocity gradients

> constant-density fluid,  $\rho(x,y,z,t) = const.$ 

- **→** barotropic
- <u>conservative</u> volume forces

$$\vec{F} = -\vec{\nabla}\Phi$$

![](_page_17_Picture_9.jpeg)

#### **Balance and evolution equations**

## Conservation of mass ("continuity")

![](_page_18_Figure_2.jpeg)

#### Navier-Stokes equation

$$\frac{D\vec{u}}{Dt} = -\frac{1}{\rho}\vec{\nabla}p' + v\,\Delta\vec{u}$$

## Vorticity equation

$$\frac{D\vec{\omega}}{Dt} = (\vec{\omega} \cdot \vec{\nabla})\vec{u} + v\,\Delta\vec{\omega}$$

$$\Delta = \nabla^{2}$$
Laplacian
$$\frac{D}{Dt} = \frac{\partial}{\partial t} + (\vec{u} \cdot \vec{\nabla})$$
material derivative
$$p' = p + \rho \Phi$$
p: pressure
v: kinematic viscosity

![](_page_18_Picture_8.jpeg)

Laws and theorems

#### Biot-Savart relation

$$\vec{u}(\vec{r},t) = -\frac{1}{4\pi} \int_{V} \frac{(\vec{r} - \vec{r}') \times \vec{\omega}(\vec{r}',t)}{|\vec{r} - \vec{r}'|^{3}} d^{3}r'$$

> Kelvin's Theorem for an ideal fluid (v = 0)

"The circulation of any closed material line is conserved during its motion"

![](_page_19_Figure_5.jpeg)

- Theorems and laws of Lagrange and Helmholtz
- → <u>summary</u>: In an ideal fluid, the circulation of each fluid element is constant in time and advected by the velocity field

![](_page_19_Picture_8.jpeg)

#### **Vortices**

- local concentration of vorticity
- (fairly) axisymmetric
- tube-like structure

• circulation  $\Gamma$ 

• core radius a

![](_page_20_Picture_4.jpeg)

• Reynolds number  $Re = \Gamma / v$ 

![](_page_20_Figure_5.jpeg)

![](_page_20_Picture_6.jpeg)

![](_page_21_Figure_0.jpeg)

![](_page_21_Picture_1.jpeg)

![](_page_22_Figure_0.jpeg)

- calculate  $\vec{u}(\vec{r}(l)) = \vec{u}_{ext} + \vec{u}_{int}$
- using Biot-Savart
  - $\vec{\omega}d^3r' \rightarrow \Gamma d\vec{l}$

$$\vec{u}_{ind}(\vec{r},t) = -\frac{\Gamma}{4\pi} \int_{L} \frac{(\vec{r}-\vec{r}') \times d\vec{l}}{\left|\vec{r}-\vec{r}'\right|^{3}}$$

![](_page_22_Picture_5.jpeg)

#### Vortex filaments

**Problem:** 

- singularity for  $\vec{r} = \vec{r}'$ 

#### Solution:

- reconsider finite core size *a*
- $-a \ll R_o$ ,  $a \ll L$

$$\Gamma$$

$$r$$

$$r(l)$$

$$r(l)$$

$$\vec{u}_{ind}(\vec{r},t) = -\frac{\Gamma}{4\pi} \int_{L} \frac{(\vec{r}-\vec{r}') \times d\vec{l}}{\left|\vec{r}-\vec{r}'\right|^{3}}$$

![](_page_23_Picture_8.jpeg)

**Vortex filament evolution** 

Local Induction Approximation

![](_page_24_Figure_2.jpeg)

![](_page_24_Picture_3.jpeg)

Flow around a wing (1)

**Circular cylinder in 2D (degenerated wing)** 

• potential flow ( $\vec{\omega} = 0$  everywhere)

![](_page_25_Picture_3.jpeg)

without circulation

ho force
 on cylinder

![](_page_25_Picture_6.jpeg)

with circulation,  $|\Gamma| < 4\pi Ua$ 

 $\textbf{ift force} \\ L = \rho \ U \ \Gamma$ 

![](_page_25_Picture_9.jpeg)

#### Flow around a wing (2)

#### Airfoil at incidence in 2D

![](_page_26_Figure_2.jpeg)

![](_page_26_Picture_3.jpeg)

Flow around a wing (3)

#### Airfoil at incidence in 2D

![](_page_27_Picture_2.jpeg)

#### starting vortex behind an impulsively translated airfoil (Prandtl & Tietjens 1934)

![](_page_27_Picture_4.jpeg)

Flow around a wing (4)

3D (rectangular) airfoil (finite wing span)

![](_page_28_Figure_2.jpeg)

#### 

![](_page_28_Picture_4.jpeg)

Flow around a wing (5)

Global vortex system of a finite-length airfoil in motion

![](_page_29_Figure_2.jpeg)

![](_page_29_Picture_3.jpeg)

#### Flow around a wing (6)

#### **Non-rectangular wing**

![](_page_30_Figure_2.jpeg)

# • distribution Γ(y) not constant

 shedding of a vorticity sheet
 between y = 0 and y = B/2

• circulation density  $\gamma(y) = d\Gamma / dy$ 

![](_page_30_Figure_6.jpeg)

![](_page_30_Picture_7.jpeg)

#### Vortex system in the wake of a civil aircraft – typical take-off/landing configuration – (including horizontal tail plane)

![](_page_31_Figure_1.jpeg)

![](_page_31_Picture_2.jpeg)

#### Vortex system in the wake of a civil aircraft

- typical take-off/landing configuration -

![](_page_32_Figure_2.jpeg)

![](_page_32_Picture_3.jpeg)

#### Vortex system in the wake of a civil aircraft

- typical take-off/landing configuration -

![](_page_33_Figure_2.jpeg)

![](_page_33_Picture_3.jpeg)

#### Dynamics of two point vortices - same circulation -

![](_page_34_Figure_1.jpeg)

![](_page_34_Picture_2.jpeg)

## Dynamics of two point vortices

- different circulations -

![](_page_35_Figure_2.jpeg)

![](_page_35_Picture_3.jpeg)

#### **Vortex pair parameters**

![](_page_36_Figure_1.jpeg)

rate of strain induced by one vortex on the other:  $\varepsilon = \Gamma / 2\pi b^2$  ( $\varepsilon^* = a^2/b^2$ )

![](_page_36_Picture_3.jpeg)

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![](_page_37_Picture_11.jpeg)

![](_page_38_Figure_0.jpeg)

![](_page_38_Figure_1.jpeg)

![](_page_38_Picture_2.jpeg)

#### **2D merging** (*Re* = 500–2500)

![](_page_39_Figure_1.jpeg)

![](_page_40_Figure_0.jpeg)

![](_page_40_Picture_1.jpeg)

#### The mechanism of merging

![](_page_41_Figure_1.jpeg)

![](_page_41_Picture_2.jpeg)

#### **Asymmetric 2D merger**

![](_page_42_Figure_1.jpeg)

$$\Gamma_2 / \Gamma_1 = 0.25; a_2 / a_1 = 0.5$$

![](_page_42_Picture_3.jpeg)

![](_page_42_Picture_4.jpeg)